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DOI:

[10.1111/jce.12991](https://doi.org/10.1111/jce.12991)

Document Version

Peer reviewed version

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Citation for published version (APA):

Chen, Z., Cabrera-Lozoya, R., Relan, J., Sohal, M., Shetty, A., Karim, R., Delingette, H., Gill, J., Rhode, K., Ayache, N., Taggart, P., Rinaldi, C. A., Sermesant, M., & Razavi, R. (2016). Biophysical Modelling Predicts Ventricular Tachycardia Inducibility and Circuit Morphology: A Combined Clinical Validation and Computer Modelling Approach. *Journal of Cardiovascular Electrophysiology*, 27(7), 851-860.
<https://doi.org/10.1111/jce.12991>

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Biophysical modelling predicts ventricular tachycardia inducibility and circuit morphology: A combined clinical validation and computer modelling approach

Short title:

VT stimulation *in silico*

Zhong Chen MBBS^{1,2}, Rocio Cabrera-lozoya PhD³, Jatin Relan PhD³, Manav Sohal MBBS^{1,2}, Anoop Shetty MD^{1,2}, Rashed Karim PhD¹, Herve Delingette PhD³, Jaswinder Gill MD^{1,2}, Kawal Rhode PhD¹, Nicholas Ayache PhD³, Peter Taggart DSc⁴, C Aldo Rinaldi MD^{1,2}, Maxime Sermesant PhD³, Reza Razavi MD^{1,2}

Institutions:

1. Kings College London, London, United Kingdom
2. Guy's and St Thomas' Hospital, London, United Kingdom
3. Inria, Asclepios Team, Sophia Antipolis, France
4. University College Hospital, London, United Kingdom

Corresponding author

Dr. Zhong Chen, King's College London, Department of Imaging Science and Biomedical Engineering, The Rayne Institute, 4th Floor Lambeth Wing, St. Thomas' Hospital Campus, London SE1 7EH

This article has been accepted for publication and undergone full peer review but has not been through the copyediting, typesetting, pagination and proofreading process, which may lead to differences between this version and the [Version of Record](#). Please cite this article as [doi: 10.1111/jce.12991](#).

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Z. Chen, R. Cabrera-lozoya and J. Relan contributed equally to the production of the manuscript.

This research received funding from the European Community's Seventh Framework Programme (FP7/2007-2013) under grant agreement n 224495 (EU-Heart project) and the ERC advanced Grant MedYMA 291080. The work was supported by the National Institute for Health Research (NIHR) Biomedical Research Centre at Guy's and St Thomas' NHS Foundation Trust and King's College London.

Z. Chen received an investigator-led research grant from Medtronic Ltd and Clinical Research Training Fellowship grant from the British Heart Foundation. Other authors: No disclosures.

Abstract

Introduction: Computational modelling of cardiac arrhythmogenesis and arrhythmia maintenance has made a significant contribution to the understanding of the underlying mechanisms of arrhythmia. We hypothesized that a cardiac model using personalized electro-anatomical parameters could define the underlying ventricular tachycardia (VT) substrate and predict reentrant VT circuits. We used a combined modelling and clinical approach in order to validate the concept.

Methods and results: Non-contact electroanatomic mapping studies were performed in 7 patients (5 ischemics, 2 non-ischemics). Three ischemic cardiomyopathy patients underwent a clinical VT stimulation study. Anatomical information was obtained from cardiac magnetic resonance imaging (CMR) including high-resolution scar imaging. A simplified biophysical mono-domain action potential model personalized with the patients' anatomical and electrical information was used to perform *in silico* VT stimulation studies for comparison. The personalized *in silico* VT stimulations were able to predict VT inducibility as well as the macroscopic characteristics of the VT circuits in patients who had clinical VT stimulation studies. Patients with positive clinical VT stimulation studies had wider distribution of action potential duration restitution curve (APD-RC) slopes and APDs than patient 3 with a negative VT stimulation study. The exit points of reentrant VT circuits encompassed a higher percentage of the maximum APD-RC slope compared to the scar and non-scar areas, 32%, 4% and 0.2% respectively. **Conclusions:** VT stimulation studies can be simulated *in silico* using a personalized biophysical cardiac model. Myocardial spatial heterogeneity of APD restitution properties and conductivity may help predict the location of crucial entry/exit points of reentrant VT circuits.

Keywords: Ventricular tachycardia; computer modelling; APD restitution; conductivity; cardiac magnetic resonance imaging.

Introduction

Implantable cardioverter defibrillator (ICD) shocks are a cause of substantial morbidity in patients with ventricular arrhythmias.¹ Radiofrequency ablation is increasingly used to treat ventricular tachycardia (VT) to reduce ICD discharges and improve patient quality of life and mortality.^{2,3} The current arrhythmia risk stratification strategy is imperfect and is determined largely on left ventricular (LV) function with not all high-risk patients receiving an ICD, and those who received ICDs never experiencing appropriate therapies. Similarly ablation of VT is technically challenging with a recurrence rate of up to 40% with a lack of clinical consensus on the optimal ablation strategy.⁴ Better risk stratification and higher ablation success rates would potentially improve patient outcomes. There is therefore a need to identify individuals at high risk of developing ventricular arrhythmia and the arrhythmia substrate in order to guide the optimal ablation strategy.⁵

Computational modelling of cardiac arrhythmogenesis and arrhythmia maintenance can be used to contribute to the understanding of the underlying mechanisms of arrhythmia. Image-based computational models have incorporated cardiac structural information such as heterogeneity of scars into such simulations.⁶⁻⁸ However, the heterogeneity in action potential duration (APD) restitution, the adaptation of APD as a function of the cardiac cycle length, has a crucial role in arrhythmogenesis.^{9,10} The integration of both personalized structural and functional data has not previously been performed.

We hypothesized that, using personalized electrophysiological mapping data and structural anatomical data acquired respectively from electrophysiology studies and high-resolution cardiac magnetic resonance imaging (CMR) we could develop a patient-specific biophysical model to perform *in silico* VT stimulation studies to assess inducibility of VT and circuit morphology.

Methods

Patients

Patients under consideration for primary prevention ICD on the basis of their LV function were prospectively invited to participate in the study following local research ethics committee approval. Seven patients, 5 with ischemic cardiomyopathy (ICM) and 2 with non-ischemic dilated cardiomyopathy (NICM) gave written consent prior to study inclusion.

CMR Acquisition and Image Processing

CMR was performed on a Philips Achieva 1.5T scanner using a 32 channel cardiac coil. All 7 patients completed CMR morphological and volumetric assessment as well as high-resolution scar characterization by late-gadolinium-enhanced (LGE) imaging with acquired voxel size $1.3 \times 1.3 \times 2.6 \text{ mm}^3$. A personalized 3D model of the ventricles was derived from the CMR images: a tetrahedral mesh was generated from the binary mask of the ventricles. The LV myocardial scar distribution was segmented using signal intensity (SI) based analysis from the high-resolution LGE images to distinguish between scar core and gray zone. Each element of the mesh was labelled (healthy/scar core/gray zone).

(Details of CMR image acquisition protocol and imaging processing data is provided in the online supplemental material)

Invasive Electrophysiological Study with Electroanatomic Mapping and Signal Processing

LV electroanatomic mapping (EAM) was performed using a multi-electrode array catheter (EnSite Velocity System, St Jude Medical, MN, USA) in all 7 patients. The chamber geometry was reconstructed using locator signals from a steerable electrophysiological catheter. Three patients (patients 1-3) with ICM underwent a simultaneous VT stimulation study according to the Wellens

protocol during the mapping study.¹¹ Unipolar electrograms (UEG) derived were filtered with a band-pass filter (10Hz/300Hz and 0.5Hz/30Hz) to optimize QRS complex and T wave detections. The depolarization times were detected within the QRS window and derived from the zero crossings of the laplacian of the measured UEGs; the repolarization times were detected within the ST window for the signals.⁹ The difference between the depolarization and repolarization times was used to estimate the activation recovery time (ARI) that is used as a surrogate marker for APD.¹² The APD restitution curve (APD-RC) was estimated from steady-state RV pacing (500ms) with sensed pacing extras at progressively shorter coupling interval at a decrement of 20ms till 200ms or refractory period. The APD-RC was represented by a non-linear equation using a least-squares fit to the mono-exponential function as previously detailed on experimental and clinical data: a single APD-RC was fitted for each measured point from the EAM and the maximum APD was estimated as the asymptotic APD of the APD-RC when the diastolic interval tends to infinity.^{13,14}

Construction of Personalized 3D Cardiac Model

Building on the framework that we have previously described and validated, the anatomical mesh was registered with the electrical information offline and used to generate a personalized 3D cardiac model, which combines the benefits of an Eikonal (EK) model (fast and robust for conduction velocity (CV) personalization) and those of a simplified biophysical mono-domain action potential Mitchell-Schaeffer (MS) model (well suited for personalising APD restitution properties).¹³⁻¹⁵ The MS model was personalized with the apparent conductivity (AC) values derived from the patient's CV computed from the EAM data. AC is the diffusion coefficient that represents an intrinsic parameter of the cardiac tissue electrical conductivity in the electrophysiological cardiac model. $AC (m^2s^{-2})$ is proportional to the product of the square of CV and a time constant parameter in the model.⁸ AC is used as an independent estimation of the intrinsic biophysical electrical conductivity property of the tissue rather than CV that could be dependent on the activation sequence and the shape of the

propagation wave front. The process of building the models from the CMR and EAM data is illustrated in Figure 1.

(The estimation of the electrical parameters and computer modelling is described in detail in the Supplemental material: Computer modelling)

In silico VT Stimulation Study

In 3 patients (patients 1-3) with ICM, the personalized cardiac model was used to simulate a clinical VT stimulation study *in silico* in order to predict the initiation and maintenance of ventricular arrhythmia induced during clinical study. The simulated study was performed in accordance with the clinical study protocols that were carried out: the pacing stimuli were applied from the RV apex following the Wellens protocol. We also simulated the study from alternate pacing sites in the RV and LV that encompassed the basal and apical freewall/lateral/septum/anterior and inferior walls. The exit points identified from the clinical VT stimulation studies and the *in silico* simulations were characterized in terms of the spatial heterogeneities of the AC, APD restitution properties.

Statistical analysis

The electrical parameters consisted of multiple data points, each corresponding to a different location within the LV of an individual patient. The data were expressed by median and inter-quartile range (IQR) or mean and standard deviation. Continuous variables were compared using Median test. A p value < 0.05 was considered to be statistically significant. All statistics were performed using computer software SPSS Statistics, version 21, SPSS Inc., IBM, USA.

Results

All 7 patients underwent successful validation of the personalization strategy of the computer cardiac

model. Of these, 3 patients (ICM) underwent further clinical VT stimulation test in order to validate the accuracy of the personalized cardiac model in predicting VT substrate.

Baseline patient characteristics and CMR findings are summarized in Table 1. During the clinical VT stimulation studies, patients 1 and 2 developed sustained monomorphic VT; patient 3 was non-inducible. All 7 patients were implanted with ICDs for primary prevention following clinical assessment. During a median follow-up period of 22 months, IQR 9 months, patient 2 received appropriate ICD therapy for sustained VT.

Heterogeneities in Apparent Conductivity (AC) and APD Restitution Properties

The IQRs of AC and APD restitution data representing the heterogeneities of these electrical parameters were calculated for each patient (shown in online supplementary Figure 1). The range of AC across the LV was comparable across the 7 patients. The median APD-RC slopes and maximum asymptotic APD for NICM patients was lower than that for ICM patients ($p < 0.01$). Amongst the 3 patients who underwent a clinical VT stimulation study, patients 1 and 2 with positive clinical VT stimulation studies had APD-RC slopes IQRs of 1.50 and 1.02; and maximum asymptotic APD IQRs of 123ms and 66ms. These IQRs were greater than that of patient 3 with a negative clinical VT stimulation study; in whom the APD-RC slope IQR and APD IQR were 0.48 and 36ms, respectively.

The APD-RC properties and ACs are also illustrated with LV polar plots to provide a qualitative assessment of the spatial heterogeneity of these parameters across the LV in Figure 2.

There appeared to be the same broad spatial heterogeneity in AC in all the study patients including the 2 patients with NICM who also had regions of low AC in areas without scars seen on CMR. However, there was a wide variation in the spatial heterogeneity of APD-RC properties across the cohort, with patients 1 and 2 showing the most heterogeneity.

Visually, the VT exit points that were observed during the clinical VT stimulation studies in patients 1 and 2 appear to be at the neighboring regions with varying degree of APD-RC properties and AC. These VT exit points were in the scar border zone/gray zone as determined by the LGE CMR scans. In order to explore the role of local spatial heterogeneity of electrical properties play in arrhythmogenesis we assessed the differences in AC, APD and APD-RC between neighboring regions in LV (each region $\approx 3\text{mm}^3$) by evaluating the gradient of the parameters in polar coordinates in Figure 2. The gradient amplitude reflects how smooth or abrupt the transition is between values in the spatial domain. Using a definition of “high gradient” being greater than the 90th percentile of the gradient range, the proportion of LV regions with high gradients was analyzed for each patient. For each of the electrical parameters, AC, APD and APD-RC, there was no statistically significant difference in the number of elements with high gradients (≥ 90 percentile) between patients. However, patient (1 and 2) with inducible VT had a combined greater heterogeneity of both AC and APD-RC, shown in Figure 3.

Induction of VT and Clinically Observed Monomorphic VT Exit Points

Patient 1 had induced sustained monomorphic VT (SMVT) with a cycle length (CL) of 275ms at Wellens’ stage 11. Patient 2 had induced SMVT with a cycle length of 245ms at Wellens’ stage 4. The patterns of activation for both reentrant VT circuits are illustrated in Figure 4. Analysis of the UEG recording from the EAM showed a higher percentage of maximum APD-RC slope that is 2 standard deviation (*SD*) above the mean LV APD-RC slope at the observed exit points (32%) compared to the scar (4%) and non-scar regions (0.2%). The absolute values in APD and tissue conductivity between the three areas were not as distinct although the exit point values (APD: median 319ms, IQR 45ms; AC: median $3.4\text{m}^2\text{s}^{-2}$, IQR $2.5\text{m}^2\text{s}^{-2}$) appeared to lie between those of the scar

(APD: median 385ms, IQR 136ms; AC: median $0.4\text{m}^2\text{s}^{-2}$, IQR $2.1\text{m}^2\text{s}^{-2}$) and non-scar regions (APD: median 305 IQR 49ms; AC: median $4.7\text{m}^2\text{s}^{-2}$, IQR $2.4\text{m}^2\text{s}^{-2}$). It is possible that it is the heterogeneity in regional tissue electrical properties distributions rather than the absolute value (mean or median) that may allow us to identify the exit points from other regions of the myocardium.

Comparison of Model-Predicted and Clinically-Observed Induced VT

Sustained monomorphic VT was induced *in silico* at stage 7 of the virtual Wellens protocol for Patient 1 and stage 5 for patient 2. Sustained VT was not inducible in *in silico* for patient 3. LV polar plots of the clinical and virtual VT isochrones are illustrated in Figure 5A for comparison. Both macroscopic reentrant VT circuit and exit points were matched between the clinical and simulated studies (shown in Figure 5A).

Three-Dimensional VT Circuit Visualization

By taking into account the 3D geometric information including transmural scar core and gray zone across the LV wall, the computer model enabled the prediction of a 3D VT circuit as opposed to the 2D VT activation pattern observed by endocardial EAM. Computational simulation allowed this additional insight to the wave propagation within the myocardium. For patient 2, the activation wave front of the reentrant VT is shown propagating in the region of the gray zone in Figure 5B. The estimated wave front path surrounds the scar core and lies within the scar border zone, entering from the endocardial surface, meandering within the ventricular wall, and exiting via the epicardial surface (shown in Figure 5B).

A comparison of clinically observed and predicted exits points in terms of anatomic location were made. We defined the exit region compassing anatomical points with an activation time within 10ms of the earliest activation. The distance between the clinically observed and simulated exit points was

defined as the 3D Euclidean distance between the centers of both exit regions. A difference of 7mm and 8mm were found, respectively, for patients 1 and 2.

Simulated VT Stimulation from Additional Sites

VT stimulation study was also performed *in silico* by pacing from other sites than the RV apex used during the clinical study for patients 1 and 2. Different VT circuits with three additional exit points were observed in both patients. The exit points were located on the boundary of scar in the region of the gray zones from the CMR LGE images. Similar to the clinically observed exit points, they were mostly in the region of maximum APD-RC slope. The composite of different exit points are plotted in Figure 6 in terms of their APD restitution properties and AC.

Discussion

The present study provides new insights into the prediction of VT circuits using a biophysical model. The principal findings of our study are as follows: 1) the location of scar border zone (gray zone) on high-resolution CMR correlates with areas of abnormal measured and model derived electrical properties; 2) the VT exit points have a substantially higher percentage of tissue with steep APD-RC slopes compared to surrounding tissues; and combined tissues heterogeneity in APD-RC and CV may underlie the substrate for the inducibility of VT; 3) *in silico* VT stimulation studies were able to predict inducibility of VT in patients at risk of ventricular arrhythmia; 4) the characteristics of the modeled VT circuits correlated well with the clinically observed circuits in terms of cycle length, macroscopic activation patterns and VT exit sites.

Tissue Heterogeneity (admixture of scar and myocardium) co-location with Heterogeneity in APD Restitution Properties and Tissue Conductivity

A correlation between the spatial heterogeneity in APD, APD-RC slopes and AC and the location of gray zone detected on high-resolution CMR supports the notion that myocardial scars can alter the regional restitution properties and provide potential substrate for arrhythmia.¹⁶ Data from the 2 patients who developed sustained VT suggest that VT exit points are co-located with heterogeneous APD-RC slopes. Ciaccio *et al.* has demonstrated potential mechanisms using a geometric model that could account for this co-location between exit zones and conducting channels in terms of tissue conductivity.¹⁷ The presence of clumps of fibroblasts, although electrically non-excitable, results in a slowing of the electrical wave front propagation in the myocardial tissue in which they are embedded. Fibroblasts can modulate cellular ion channel remodelling and therefore tissue electrical properties through a variety of mechanisms including mechano-electric feedback via stretch-activated ion channels, close coupling of nearby cardiac myocytes via connexin, and by altering surrounding myocardial fibres anisotropy.¹⁸ Some of these mechanisms have been shown in vitro, but remains speculative in vivo. The suggested relationship between the degree of heterogeneity demonstrated by the electrical gradients between neighboring tissue domains and the propensity for sustained ventricular arrhythmia is therefore likely being non-linear as observed in the present study. The present study supports the notion that potential successful ablation sites for VT lie in areas of heterogeneous tissue zones that can be identified with CMR.^{19,20}

Heterogeneity in electrical properties have been observed in LV.^{9,10} Computation modelling have demonstrated that theoretically APD-RC slope >1 is needed to result in electrical instability and initiate ventricular arrhythmia.²¹ In keeping with the observed tissue functional heterogeneity at the VT exit points in the present study, others have also demonstrated that the heterogeneity in APD-RC slopes is needed for the initiation and stability of reentry VT.^{10,22} These prior studies did not have the

benefit of high-resolution CMR scar information, and so could not explain the anatomical cause of this. Nash *et al.* speculated that regional stretch strain pattern resulting from ischemia might have led to electrical remodelling through mechano-electric feedback.¹⁰ It may well have been that these regions had areas of gray zone as they correlated to the territories of the diseased coronary arteries.

***In silico* VT stimulation studies in patients**

Encouragingly, the personalized cardiac models encompassing both anatomical and electrical properties were able to predict not only the inducibility of VT, but also the reentrant VT circuit properties and anatomical locations of the substrate. The present study is unique in that, as well as anatomical and scar information it incorporated personalized functional data including APD-RC properties and tissue conductivities into the patient-specific cardiac models. Previously, Arevalo H *et al.* suggested that VT dynamics were primarily governed by the geometric parameters of the scar-core and border zone using image-based computational VT modelling work.⁷ The present study highlighted the advantage of incorporating detailed geometric information gained from CMR, demonstrating the possibility of using high-resolution 3D scar data to help predict potential critical isthmus on the epicardial surface. This is important, as conventional mapping techniques used during ablative therapy are limited to two-dimensional geometry when the substrate of the VT circuit could be on the opposite side of the mapping surface.

While we realize that CMR can provide important scar geometry that governs the substrate of reentrant VT, we also recognize that the resolution of the current standard clinical CMR technique is limited (common voxel size 2x2x8mm³) in providing the level of spatial geometry details that we would like to see at the border zone. We believe that additional knowledge and understanding of patient-specific heterogeneities in local electrical parameters would assist in predicting the likely culprit conduction channels/isthmus, and not the bystanders, that is critical to the clinical VT. We

have performed additional sensitivity analysis using empirical electrical parameters instead of personalized patient-specific electrical data in the 2 patients with positive clinical VT stimulation studies and found that using combined personalized electrical and image data can potentially improve the accuracy of VT inducibility and predictions regarding the location of exit zones predictions. VT was not inducible in Patient 1 using non-personalized empirical electrical parameters that also induced a different macroscopic VT circuit morphology from the one seen during the clinical study in Patient 2. The Euclidean distance between the center of the clinical exit region and that predicted using non-personalized electrical parameters was 37mm, and with using personalized electrical parameters it was 8mm. (See Supplemental Material: Personalized vs. non-personalized empirical electrical parameter) However, recognizing the small number of patients included in this analysis, a larger study would be necessary to help draw more reliable conclusions between using personalized vs. non-personalized electrical parameters.

Clinical application: Potential for Circuit Prediction using Personalized Computer Models to Guide Ablation

While cardiac modelling has been an active research area for decades, personalized cardiac modelling using patient-specific clinical data is in its infancy. *In silico* personalized models may offer significant clinical benefit in predicting the risk of ventricular arrhythmia in patients and guiding treatments including ICD implantation and VT ablation. Successful VT termination through ablation may be achieved when the critical isthmus is successfully interrupted with ablation lesions. If VT exit points can be predicted with biophysical models, then this information may be used to guide ablation. Such models also offer additional flexibility as the model can simulate any combination of paced stimuli from different locations with varying pacing cycle lengths, which may not be feasible in clinical practice. Recently, Ashikaga *et al.* presented a retrospective study that found a good correlation between the predicted ablation sites and the actual target VT ablation sites at the scar border zone.²³

We have indeed demonstrated that additional exit points can be induced from *in silico* VT stimulation studies, which could be potential targets for ablation. Our results suggest that patient-specific cardiac models may offer incremental clinical benefit in terms of ventricular arrhythmia risk stratification and in the planning and delivery of ablation strategies for reentrant ventricular arrhythmias. Non-invasive body surface mapping could be incorporated to routine simple electrophysiology study to gain such personalized whole heart electro-anatomic data in order to facilitate the translation of the biophysical cardiac model processing pipeline to clinical practice.²⁴ A larger validation study can be performed in the secondary prevention patient cohort when simple electrophysiology study can be performed via the cardiac rhythm management device (at time of device implant) with simultaneous body surface mapping recording to acquire the personalized APD, APD-RC slopes and AC data. This coupled with scar data acquired from CMR prior to device implant could generate personalized modelling, the outcome of which can then be further validated at the time of VT ablation prospectively in this secondary prevention cohort

Study limitations

Given the invasive nature of the study precludes analysis of a large number of patients, the study is limited by the small number of patients included with only a subset of patients undergoing a VT stimulation procedure. The electro-anatomical data are derived from non-contact mapping with the inherent limitations of this type of mapping. It was chosen for its ability to provide ‘beat-to-beat’ mapping in the setting of rapid and unstable VT circuits. The registrations between the electroanatomic mapping and CMR scar mapping and between the clinical and in-silico data are performed through anatomical landmark registration. Though this is a simple but effective way of registration, it is susceptible to arbitration. This process can be further refined through a deformable registration method that has the advantage of improved reproducibility, however at the expense of introducing systematic error with resultant over-fitting.²⁵ The cardiac model also made several simplifications in particular for the Purkinje network and pathological changes of cardiac fiber

orientations. With any personalization of computational physiology model, there is a degree of uncertainty due to the limitations in acquired temporal and spatial resolution clinical data. Extending computational methods used in the study to incorporate an efficient Bayesian inference method could account the uncertainties in the application of the model.²⁶

Conclusion

Patient-specific spatial heterogeneity of restitution properties were the distinguishing features of ventricular arrhythmogenicity, with reentrant VT exit points present in regions of higher maximum APD-RC slopes compared with the surrounding tissue. These regions were within the gray zone identified by LGE CMR. Personalized biophysical model was able to predict macroscopic VT circuits and exit point locations in agreement with clinically observed datasets.

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Figure 1 (A) high-resolution contrast-enhanced CMR scar images; (B) whole heart model segmented from 3D steady-state free precession (SSFP) CMR with scar (core and gray zone) in violet; (C) low voltage areas from electroanatomical mapping. Lower panel: (D) model personalization and *in silico* VT stimulation study procedure workflow.

The above figure describes the study protocol and workflow of the data analysis. High-resolution CMR images (A) provided an accurate structure of the cardiac model, incorporating scar details including scar core and score border zone (gray zone) (B). Additional whole heart (LV) electrical parameters such as APD, APD restitution properties and conductivity (C) are acquired through electrophysiology studies and incorporated into the model personalization (D). VT stimulation study is performed clinically and *in silico* in parallel on a subset of patient cohort to allow a comparison of outcomes. The electrical parameters at the site of VT exit points are analyzed to assess the characteristic features that would support the arrhythmia substrate.

Figure 2. LV polar plot representation of the spatial distribution of the maximum slope for APD-RCs, maximum asymptotic APD and AC.

Scars identified by LGE CMR with its border zone (highlighted by gray contours) and clinically observed exit points (highlighted in Patient 1 and 2 by fang-shaped* white contours during reentrant VT) are overlaid to the polar plots.

*Fang-shaped due to unfolding of 3D volume surface to 2D polar plot)

Figure 3. Percentages of LV spatial domains with high gradient (> 90th percentile of the gradient range) as a representation of spatial differences between neighboring regions in terms of AC and APD-RC slope for each patient (P1-P7).

The separating line with a maximal margin was computed here using the Support Vector Machine algorithm.

Figure 4. Isochrones map during reentrant VT.

(A) Patient 1 with VT cycle length 275ms; (B) Patient 2 with VT cycle length 245ms. In Patient 1, the sustained VT self-terminated 42 seconds after failed attempts of overdrive pacing given due to patient's stable hemodynamic response. In Patient 2, the sustained VT required DC-cardioversion due to patient's unfavorable hemodynamic response. The 3D VT isochrones with exit points (red) in relation with scar core (white) and gray zone (gray) are shown in the left panels. Unipolar electrograms recording during VT are shown in the middle panels. LV polar plots of VT isochrones illustrating the direction of activation pattern are shown in the right panels. In Patient 1, the endocardial activation recorded from EAM showed the reentrant VT circuit initiating from the LV lateral wall, spreading anteriorly and then posteriorly before returning to the lateral wall. In Patient 2, the reentrant VT circuit exited from the LV infero-lateral wall, spreading antero-laterally and then towards the septum, before returning to the infero-lateral wall.

Figure 5.**A. VT isochrones of induced reentrant VT during clinical VT stimulation study (left panel) and during *in silico* VT stimulation study (right panel).**

The arrows point towards the directions of propagation. Scars (core and gray zone) are superimposed to the LV shell shown in darkened regions. The personalized model of patient 1 predicted a sustained reentrant VT circuit with a cycle length of 260ms compared with the clinically observed cycle length of 275ms with a macroscopically similar activation pattern and a predicted exit point that matched with the observed clinical one. The personalized model of patient 2 also predicted a positive VT stimulation study with a cycle length of 250ms compared with 245ms for the clinical VT. The induced VT was sustained and the reentrant pathway stable. Notably the direction of the activation pattern during the predicted reentrant VT was reversed from that observed clinically; however, the predicted exit point correlated with the clinically observed one.

B. Estimation of the intra-myocardial path between the entry and exit points during reentrant VT.

The isochrones map demonstrates estimated endocardial 2D geodesic path between the entry and exit points from electroanatomical study during clinical VT stimulation study. Estimated intra-myocardial 3D geodesic path (red line) takes into account of the scar heterogeneity from the high-resolution CMR images. The graded colors on the 3D path with blue denoting late activation and red denoting early activation illustrate the entry and exit points. The activation wave front of the reentrant VT propagates in the region of the gray zone. The estimated wave front path surrounds the scar core and lies within

the scar border zone, entering from the endocardial surface, meandering within the ventricular wall, and exiting via the epicardial surface.

Figure 6. Correlation of predicted exits points with structural heterogeneity and functional heterogeneity.

A = Patient 1. B = Patient 2. The left panel shows the isochrones for the three predicted VT circuits with fangs of white lines denoting the exit points. The middle panel demonstrates the LV scar distribution with black region denoting healthy myocardium, white region denoting the scar core and the gray region denoting the gray zone/scar boarder zone with overlying composite exit points (fanged green lines). The right panel demonstrates the electrical properties with overlying composite exit points (fanged green lines).

Tables

Table 1. Baseline patient characteristics and CMR findings.

ACE-I= angiotensin converting enzyme inhibitor; AF= atrial fibrillation; ARB= angiotensin receptor blocker; CMR= cardiac magnetic resonance imaging; EDV= end-diastolic volume; EF= ejection fraction; ICM= ischaemic cardiomyopathy; LV= left ventricle/ventricular; NICM= non-ischemic dilated cardiomyopathy; PAF= paroxysmal atrial fibrillation.

Patient	1	2	3	4	5	6	7
Condition	ICM	ICM	ICM	ICM	ICM	NICM	NICM
Gender	M	M	M	M	F	M	M
Age	73	69	64	60	65	75	81
Co-morbidities	HTN	None	HTN, AF	DM	None	AF	PAF
B-blocker	Yes	Yes	Yes	Yes	Yes	Yes	Yes
ACE-I/ARB	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Statins	Yes	Yes	Yes	Yes	Yes	No	Yes
LVEF, %	27	35	35	25	31	36	17
LVEDV, ml	199	292	245	304	185	196	285
LV mass, g	129	172	147	182	118	119	206
Scar on CMR	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Scar core, g	14	22	24	31	16	23	18
Gray zone, g	27	28	20	19	12	16	28